Multi-scale modelling of aneurysm formation - linking continuum mechanics and adaptation to signalling events

H. Schmid¹, M.Cooling² P.N. Watton³, P. Hunter² and M. Itskov¹

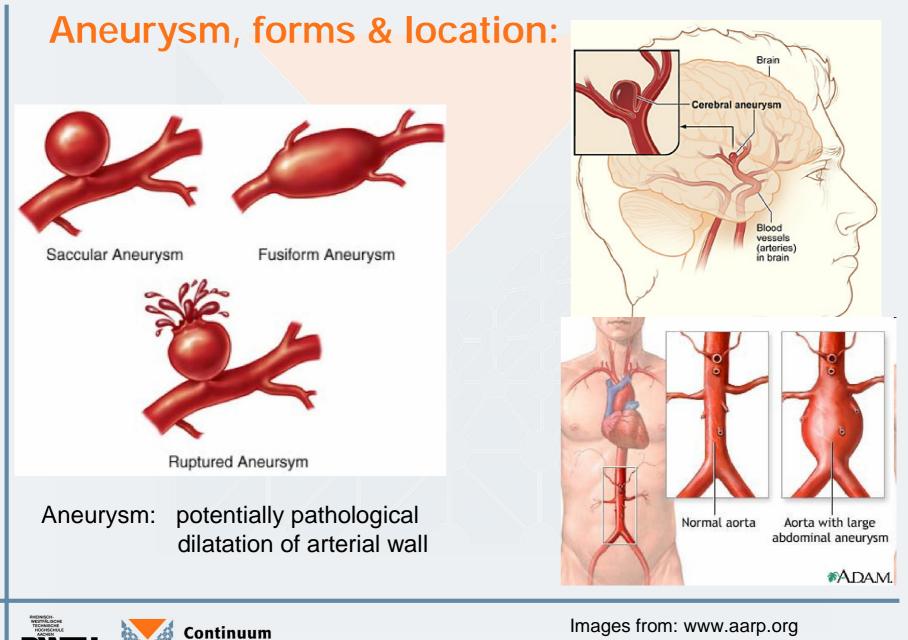
¹Department of Continuum Mechanics, RWTH Aachen University, Germany ²Auckland Bioengineering Institute, University of Auckland, New Zealand ³Department of Computational Biology, University of Oxford, Oxford, United Kingdom

26th January, 2010, CelIML meeting Auckland

Contents

- (1) Aneurysms, forms and location
- (2) Arterial micro-structure
- (3) Remodelling framework
- (4) Some basic concepts
- (5) Subsequent steps
- (6) Challenges





Arterial wall, structure:

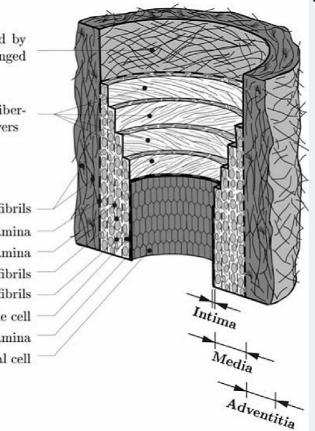
- Mechanical components:
 - smooth muscle cells
 - collagen
 - elastin

Passive & active response

Composite reinforced by collagen fibers arranged in helical structures

Helically arranged fiberreinforced medial layers

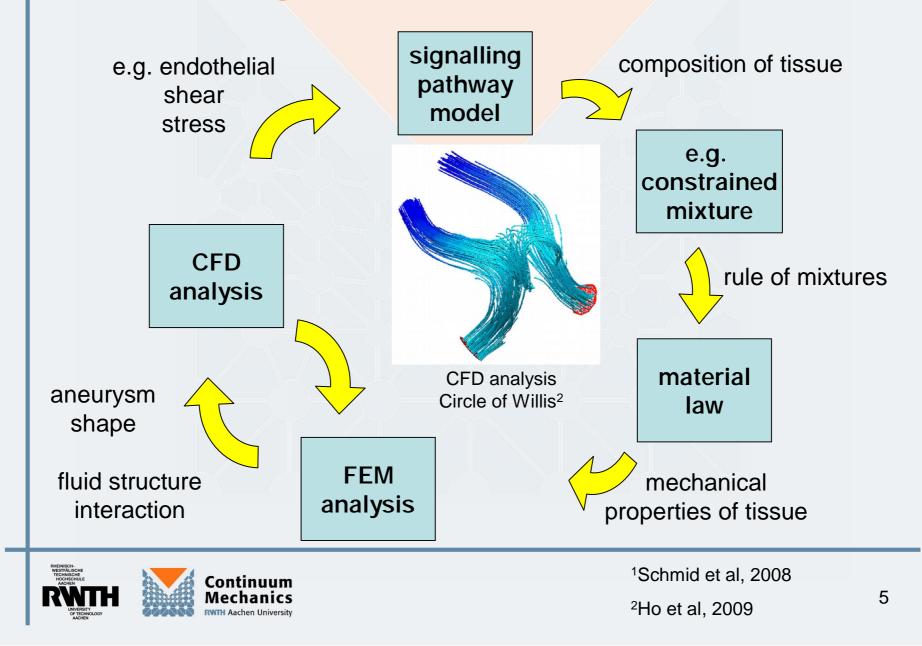
Bundles of collagen fibrils —/ External elastic lamina —/ Elastic lamina —/ Elastic fibrils —/ Collagen fibrils —/ Smooth muscle cell —/ Internal elastic lamina —/ Endothelial cell —/

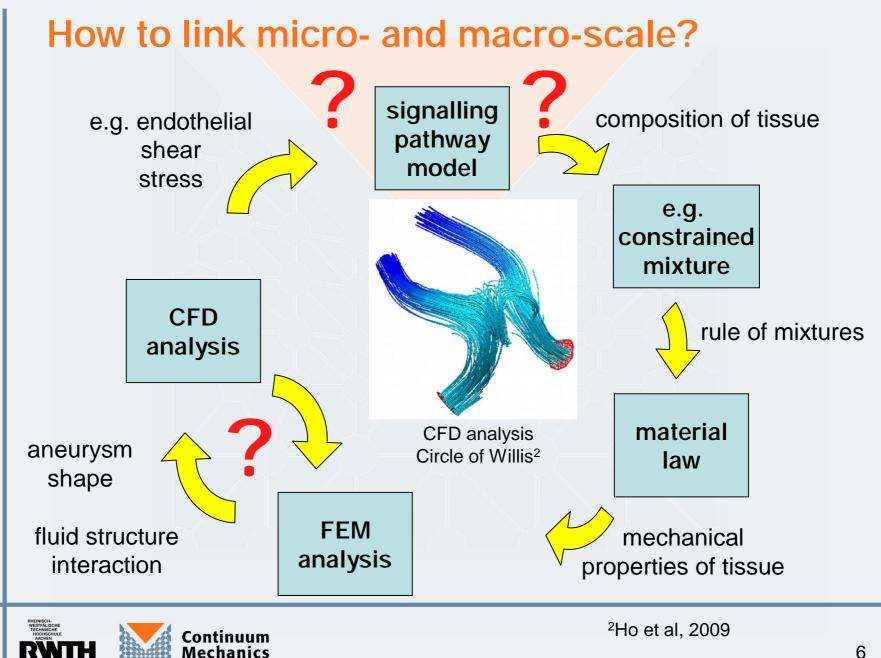




¹Holzapfel et al., 2000

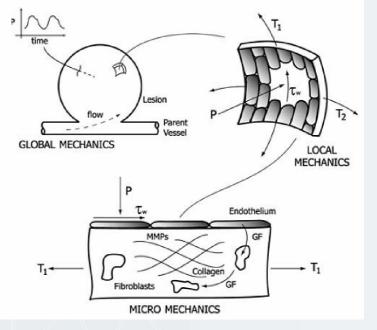
Remodelling framework¹:





Remodelling:

- Mechanical factors for altered signal transduction pathways due to change in:
 - wall shear stress (WSS) from blood flow
 - pressure biaxial stretch of endothelium
 - axial tension of artery



Possible mechanical responses to altered environment:

- active: vasoconstriction (sec ~ min)
- passive: remodelling: change of reference configuration (days ~ months)
- passive: growth: increase of constituents (days ~ months)



Current approach – just solid mechanics

 $f_e(t) = f_e(0) \ c_{\min}^{t} T$

 $\frac{\partial \lambda_{rec}}{\partial t} = \alpha (E_c - E_a)$ $\frac{\partial f_c}{\partial i} = \beta f_c (E_c - E_a)$

pressureelastin concentration collagen strainrecruitment stretch--30 -20 -10 0 10 20 30 time t



Future ideas – first step, coupling to hemodynamics

 $f_{\rho}(t) = F_{fluid}(\tau, E_{endoth})$ $\frac{\partial \lambda}{\partial t} = \alpha (E_c - E_a)$ $\frac{\partial f_c}{\partial t} = \beta f_c (E_c - E_a)$



Future ideas – second step, coupling to signalling

 $f_e(t) = F_{sign}^e(\tau, E_{endoth})$

 $\frac{\partial h}{\partial t} = F^{\lambda}_{sign}(\tau, E_{endoth})$ $\partial \lambda$

 $\frac{\partial f_c}{\partial t} = F_{sign}^c(\tau, E_{endoth})$



Challenges

- Vastly differing time scales (sec ~ years)
- Computational cost (CFD, FEM and signalling)
- How to implement it into CMISS?
 - Mechanical stress strain relationship is also implemented via CelIML
 - Problem with storage between different solution procedures
- How can we use both: the mechanical and signalling models in one integrated model?



Thank you very much for your attention!

Special thanks to

Peter

Catherine

Chris

Mike

Admin team

